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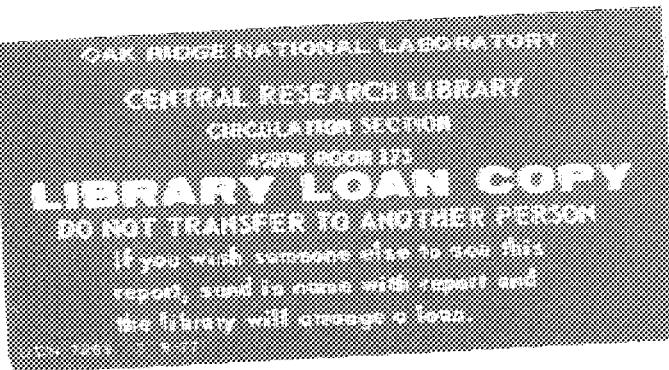
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HETFIS

High-Energy Nucleon-Meson
Transport Code with Fission

J. Barish
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ABSTRACT

A model that includes fission for predicting particle production spectra from medium-energy nucleon and pion collisions with nuclei ($Z \geq 91$) has been incorporated into the nucleon-meson transport code, HETC. This report is primarily concerned with the programming aspects of HETFIS (High-Energy Nucleon-Meson Transport Code With Fission). A description of the program data and instructions for operating the code are given. HETFIS is written in FORTRAN IV for the IBM computers and is readily adaptable to other systems.

I. INTRODUCTION

For several applications, e.g., in designing facilities to produce an intense source of low-energy neutrons by using medium-energy protons¹ and for studies of the feasibility of converting fertile-to-fissile material using medium-energy protons,² it is necessary to carry out calculations of the transport of medium- and low-energy nucleons and pions through fissionable material. In a previous paper,³ a model was developed for predicting differential particle-production data from the collisions of medium-energy nucleons and pions with fissionable nuclei ($Z \geq 91$). This model has been incorporated into the high-energy transport code, HETC.⁴ Also, in a previous paper,⁵ calculated results obtained with this updated version of HETC are compared with experimental data from medium-energy (≤ 1.47 GeV) protons incident on thick uranium targets.

This report is primarily concerned with the programming aspects of HETFIS. It is assumed here that the reader is familiar with HETC and the analysis of the history information produced by HETC. Those readers who are not should read Refs. 4 and 7 in conjunction with the present report. The program, HETC, was modified to include fission in such a way that the exclusion of the fission channel in HETFIS would produce history information for analysis that is identical to that produced by HETC. Modifications to HETC are given in Section II, data input description is given in Section III, and analysis modifications are outlined in Section IV. The HETFIS package as well as the HETC program are available from the Radiation Shielding Information Center (RSIC) at the Oak Ridge National Laboratory. Only the modified and new subroutines used to include fission in HETC are included in the HETFIS package.

II. MODIFICATIONS TO HETC

Basic changes to HETC to include fission are as follows:

- a) fission data are input via a block data routine and an auxiliary storage device on logical unit 11;
- b) several subroutines have been added and a few subroutines have been modified;
- c) the history information provided for analysis has been modified to include data from the fission process.

Listed below are the new or modified routines for use with HETFIS.

<u>Routine</u>	<u>Purpose or Changes</u>
BLOCK DATA	Contains some of the data needed for the operations of the fission channel.
DRES	Modified to include the possibility of fission.
ENERGY	Changed to obtain nearest integer value of A and integer value of Z when calling with noninteger values of A or Z.
	Includes calls to DRES to evaporate particles from fission fragments; the history information provided for analysis was modified to include data from the fission process.
FLTRN	Calls FLRAN and converts random number to single precision.
FSINFO	Fission subroutine, called when a fission occurs. The A, Z, excitation energy and kinetic energy of each fragment is calculated.

<u>Routine</u>	<u>Purpose or Changes</u>
GAMR	Calculates ratio of neutron width to fission width.
INPUTF	Fission data obtained from fitting the experimental data of Epperson ⁶ is read in. (See Ref. 3, Section III.B of this report)
INTERP	All quantities needed for subsequent call to QMAXX are obtained for nearest integer A value of either fission fragment, by interpolation in excitation energy, E_F , of fissioning nucleus.
KEAVE	All quantities needed for subsequent call to QMAXX are obtained by double interpolation in heavy fission fragment A_2 value and excitation energy, E_F , of fissioning nucleus.
PAIRR	Calculates sum of pairing energies for two fission fragments.
QMAXX	The unnormalized probability for obtaining a heavy fission fragment with given A_2 at fixed excitation energy, E_F , of fissioning neptunium nucleus is calculated.
QNRG	Changed to obtain nearest integer values of A_1 and A_2 and integer values of Z_1 and Z_2 when calling with noninteger values.
ZPROBF	Most probable noninteger values for Z_1 and Z_2 of the fission fragments are calculated.

III. DATA DESCRIPTION AND CODE OPERATION

Insofar as possible, HETFIS was designed so that operation of the code without fission would be identical to operating the HETC program. To achieve this, data for the fissioning channel are input via BLOCK DATA and an auxiliary storage device on logical unit 11. The user must also supply all data required for a normal HETC run.

A. Block Data Parameters

Many of the parameters required for using the fission channel are included in BLOCK DATA. The parameters IANLG and BZERO that occur in BLOCK DATA are user supplied. All other parameters in BLOCK DATA are permanent and should not be changed unless the user is very familiar with the statistical model of fission as used in the code and wishes to make fundamental changes in the model. The parameter IANLG is defined by

```
IANLG = 1      if the fission channel is to be used,  
              = 0      if the fission channel is not to be used,
```

and BZERO is the level density parameter (see Eq. (16) in Ref. 3). In general, BZERO should be used to be between 8.0 and 15.0. In Ref. 3 it is indicated that BZERO = 10.0 is the "best" value when fission is included and incident energies $\gtrsim 1$ GeV are considered. When fission is not included BZERO = 8.0 has usually been used in HETC.

B. Statistical Data on Auxiliary Device

To a large extent the physical data that occur in the statistical model used here have been derived from the experimental measurements of D. H. Epperson.⁶ Data tables for incident proton energies of 7, 10, 15, 20, 25 and 30 MeV have been prepared and stored on logical unit 11 to be input in subroutine INPUTF. The method used to obtain these data is

described in Ref. 3. A brief description of these data follows:

AINFO(1) = 236.0 The atomic mass of neptunium.

AINFO(2) = 93.0 The charge number of neptunium.

AINFO(3) = 92.0 The charge number for uranium.

AINFO(4) Kinetic energies of the excited neptunium compound nuclei for the six incident proton energies considered.

thru

AINFO(9)

AINFO(10) = Average excitation energies, E_F , from which fission in Neptunium for the six incident proton energies considered.

thru

AINFO(15)

AINFO(16) = 2.0 Meaningful only to code that produced data tables.

AINFO(17) = 8.0 A specific value for level density parameter BZERO. (See Eq. (16) in Ref. 3)

AINFO(18) = 1.5 A parameter, y_o , that occurs in the level density expression. (See Eq. (16) in Ref. 3)

AINFO(19) = 15.0 A specific value for level density parameter BZERO.

AINFO(20) Same as AINFO(18).

EPKIN(i,j) Relative kinetic energy of fission fragments from Neptunium as a function of 80 A (mass) values and the 6 average excitation energies.

SIGKE(i,j) Standard deviations of the EPKIN values.

DELEXC(i,j,k) Equals ΔE_c in Eq. (33) of Ref. 3. It is used to compute the total deformation energy of Neptunium fission fragments at the scission point and is a function of 80A values, six average excitation energies, and two values of B_o .

Fission data for DELEXC are supplied for BZERO = 8.0 and BZERO = 15.0.

When BZERO in BLOCK DATA is specified to be any value between 8 and 15, linear interpolation in $\frac{1}{BZERO}$ is used to obtain the required fission data.

IV. ANALYSIS CHANGES WHEN FISSION OCCURS

Since analysis of the history information supplied by HETC and HETFIS is largely left up to the user, no attempt is made here to outline an analysis of an HETFIS run. More information on the analysis procedure may be found in Ref. 7. The history information supplied for analysis is different from that supplied by HETC only if a fission occurred.

A simple "if" test allows one to determine if a fission occurred in a given collision. If a fission has occurred the values of APR and ZPR (on the history tape) for this collision are:

$$APR = 1000 * APR1 + APR2$$

$$ZPR = 1000 * ZPR1 + ZPR2$$

where

APR1 = the mass number A_1 of 1st fragment.

APR2 = the mass number A_2 of 2nd fragment.

ZPR1 = the charge number Z_1 of 1st fragment.

ZPR2 = the charge number Z_2 of 2nd fragment.

So the user only has to test APR or ZPR for a value greater than 1000 to see if fission has occurred at a particular collision.

Changes in the history information supplied (carried out in ERUP) due to fission are listed below. The general scheme is that 0.0 is placed in various arrays to separate the various types of fission information. When a fission occurs,

- 1) all current NPART(j) values for j = 1,6 are incremented by 1,

- 2) a 0.0 is stored in EPART(NPART(j),j) for j = 1,2,
to separate prefission neutrons and protons from post-
fission neutrons and protons,
- 3) a 0.0 is stored in HEPART(NPART(J+2),j) for j = 1,4,
to separate prefission evaporation light ions
(deuterons, tritons, ^3He , and alpha particles) from post-
fission evaporation light ions,
- 4) DRES is called to get evaporation products for the first
fission fragment.
- 5) all NPART(j) values for j = 1,6 are incremented by 1,
- 6) a 0.0 is stored in EPART(NPART(j),j) for j = 1,2,
to separate postfissioning evaporation neutrons and
protons produced by the first fission fragment from
postfission evaporation neutrons and protons produced by
the second fission fragment,
- 7) a 0.0 is stored in HEPART(NPART(j+2,j)) for j = 1,4, to
separate postfission evaporation light ions produced
by the first fission fragment from postfission evaporation
light ions produced by the second fission fragment,
- 8) DRES is called to get evaporation products for the second
fission fragment.
- 9) Fission fragment data are stored in the remainder of the
HEPART array for tritons (tritons should require the least
space) as follows:

I = NPART(4) + 1.

HEPART(I,2) = 0.0, separator.

HEPART(I+1,2) = ERN1, the kinetic recoil energy of
the first fragment residual after all
evaporations.

HEPART(I+2,2) = E1, the excitation energy of the
first fragment prior to evaporation.

HEPART(I+3,2) = HEVS1, sum of the kinetic energies of
all charged particles, except protons,
emitted during evaporation from the
first fragment.

HEPART(I+4,2) = USE1, the excitation energy of the
first fragment residual after all
evaporations.

HEPART(I+5,2) = ERN2, the kinetic recoil energy of
the second fragment residual after all
evaporations.

HEPART(I+6,2) = E2, the excitation energy of the
second fragment prior to evaporation.

HEPART(I+7,2) = HEVS2, sum of the kinetic energies of
all charged particles, except protons,
emitted during evaporation from the
second fragment.

HEPART(I+8,2) = USE2, the excitation energy of the
second fragment residual after all
evaporations.

HEPART(I+9,2) = HEVSO, sum of the kinetic energies of
all charged particles, except protons,
emitted during evaporation from the
original nucleus.

HEPART(I+10,2) = APR1, mass number A (after all evaporation) of the first fission fragment.

HEPART(I+11,2) = APR2, mass number A (after all evaporation) of the second fission fragment.

HEPART(I+12,2) = ZPR1, charge number Z (after all evaporation) of the first fission fragment.

HEPART(I+13,2) = ZPR2, charge number Z (after all evaporation) of the second fission fragment,

10) Stores balance of data as follows:

```
NPART(4) = NPART(4)+14  
APR = 1000*APR1+APR2  
ZPR = 1000*ZPR1+ZPR2  
EREC = ERN1+ERN2  
HEVSUM = HEVSO+HEVS1+HEVS2  
UU = USE1+USE2.
```

V. SAMPLE PROBLEM

The sample problem consisted of a 720-MeV proton beam incident on a depleted uranium cylinder surrounded by a water bath. Cylindrical geometry was used for 10 incident protons per batch and 10 batches. The

depleted uranium region was 5.1 cm in radius and 61 cm in length centered in a water bath of radius 95 cm and length of 181 cm with a void region (5.1 cm radius) for the incident proton beam in front of the uranium. Table I is a listing of source subroutine SORS and Table II is a listing of input data for the sample problem. This problem required 24.2 seconds on the IBM 370/3033 at ORNL.

VI. EDIT OF HETFIS HISTORY TAPE

Table III is a partial edit of the history tape created by running the sample problem. Two complete histories are shown. A description of such an edit is given in Ref. 7 which should be familiar to all HETC (or NMTC) users. Table III is included to demonstrate the few changes made in the history information to include fission information.

The first particle event describes a source particle and can be ignored. The second particle event describes a nuclear interaction and since APR and ZPR are greater than 1000 it has fission information. In the evaporation tables for the 6 types of particles, zero energy values are used as separators when a fission occurs. Any nonzero values prior to the first zero are the energy values of the prefission evaporation products. Any nonzero values prior to the second zero are the energy values of the postfission evaporation products from the first fission fragment. Any nonzero values after the second zero (prior to the third zero for tritons) are the energy values of the postfission evaporation products from the second fission fragment. The NPART for each type counts zero values as well as nonzero values of energies. For tritons there will be an additional 13 values for fragment data.

Table I. Subroutine SORS Listing

Table II. Sample Problem Input Data

```

720 MEV CASE----- 1CM RADIUS UNIFORM BEAM
720 MEV CASE----- 1CM RADIUS UNIFORM BEAM
121518193213
 820.0 15.00      15.00      0      -1      2      10      10      0      2
 1      0.0      1      1      0      0      59      1
 100.      3      5      1
 0.0      2      0
 92.0      238.0      4.784692E-2      0
 92.0      235.0      1.054953E-4      0
 6.691689E-2      1      1
 8.0      16.0      3.345844E-2      3
 92000      2      0      10      238.0      U DIRECTLY FROM PB
 0.10000E+09      2.56
 0.90000E+08      2.74
 0.80000E+08      2.65
 0.70000E+08      2.46
 0.60000E+08      2.13
 0.50000E+08      2.03
 0.40000E+08      2.08
 0.30000E+08      2.65
 0.20000E+08      3.63
 0.10000E+08      2.96
 92000      71      0      15      238.0      F1 U FROM PB
 0.10000E+09      0.98569E+00
 0.80000E+08      0.97576E+00
 0.70000E+08      0.96461E+00
 0.60000E+08      0.94309E+00
 0.50000E+08      0.90631E+00
 0.40000E+08      0.88482E+00
 0.30000E+08      0.90993E+00
 0.25000E+08      0.91979E+00
 0.20000E+08      0.90840E+00
 0.18017E+08      0.88497E+00
 0.17139E+08      0.87497E+00
 0.16303E+08      0.86545E+00
 0.15504E+08      0.85289E+00
 0.14751E+08      0.83890E+00
 0.10000E+08      0.83890E+00
 92000      2      0      10      235.0      U DIRECTLY FROM PB
 0.10000E+09      2.56
 0.90000E+08      2.74
 0.80000E+08      2.65
 0.70000E+08      2.46
 0.60000E+08      2.13
 0.50000E+08      2.03
 0.40000E+08      2.08
 0.30000E+08      2.65
 0.20000E+08      3.63
 0.10000E+08      2.96
 92000      71      0      15      235.0      F1 L FROM PB
 0.10000E+09      0.98569E+00
 0.80000E+08      0.97576E+00
 0.70000E+08      0.96461E+00
 0.60000E+08      0.94309E+00
 0.50000E+08      0.90631E+00
 0.40000E+08      0.88482E+00
 0.30000E+08      0.90993E+00
 0.25000E+08      0.91979E+00
 0.20000E+08      0.90840E+00
 0.18017E+08      0.88497E+00
 0.17139E+08      0.87497E+00
 0.16303E+08      0.86545E+00
 0.15504E+08      0.85289E+00
 0.14751E+08      0.83890E+00
 0.10000E+08      0.83890E+00

```

Table II. (Cont'd)

8000 2 0 13 16.00000 OXYGEN ELASTIC				JOANOU	8000 2 1
0.10000E 09	0.37000E 00				8000 2 2
0.90000E 08	0.45000E 00				8000 2 2
0.80000E 08	0.52000E 00				8000 2 3
0.70000E 08	0.61000E 00				8000 2 4
0.60000E 08	0.71000E 00				8000 2 5
0.50000E 08	0.82000E 00				8000 2 6
0.40000E 08	0.93000E 00				8000 2 7
0.30000E 08	0.10000E 01				8000 2 8
0.25000E 08	0.10200E 01				8000 2 9
0.20000E 08	0.94000E 00				8000 2 10
0.18000E 08	0.84000E 00				8000 2 11
0.15000E 08	0.74400E 00				8000 2 12
0.14750E 08	0.73500E 00				8000 2 13
				END OF 8000	2 14
8000 71 8 10 16.00000 OXYGEN ELASTIC F1				JOANOU	8000 71 1
0.10000E 09	0.96704E 00				8000 71 2
0.80000E 08	0.96057E 00				8000 71 3
0.70000E 08	0.95541E 00				8000 71 4
0.60000E 08	0.94784E 00				8000 71 5
0.50000E 08	0.93622E 00				8000 71 6
0.40000E 08	0.91607E 00				8000 71 7
0.30000E 08	0.88105E 00				8000 71 8
0.25000E 08	0.85093E 00				8000 71 9
0.20000E 08	0.80413E 00				8000 71 10
0.14750E 08	0.72100E 00				8000 71 11
				END OF 8000	71 11
2 MALE					BLANK
5.1					BLANK
95.0					BLANK
60.0	6666	2			
121.00	1	2			
181.0	2	2			

Table III. HETFIS History Tape Edit

READING LOG. 59 AS HNT TAPE

MAXBCH	MAXCAS	MAT	NGRPOL	NPIOK	NICOL	NCUT	NEXITE	NSPRED	NSPROD	NSEUDO	NBERTP					
10	10	2	2048	0	0	1	1	1	0	1	1					
EMAX 0.8200E 03																
CUTOFF ENERGIES FOR TYPES 1-7																
0.1000E 01 0.1500E 02 0.1800E 03 0.1000E 01 0.1000E 01 0.1000E 01 0.1000E 01																
MEDIUM 1																
NUCLEI NO.	Z NO.	A NO.	'GEOMETRIC' XSECT (PER CM)													
1	0.9200E 02	0.2380E 03	0.1257E 00													
2	0.9200E 02	0.2350E 03	0.2754E-03													
TRANSPORT XSECTS FOR PARTICLE TYPES 1-7 IN MEDIUM 1 IN PER CM																
0.1259E 00 0.1259E 00 0.1364E 00 0.0 0.1364E 00 0.1158E-03 0.1158E-03																
MAX HYDROGEN XSECTS FOR PARTICLE TYPES 1-5 IN MEDIUM 1 IN PER CM																
0.0 0.0 0.0 0.0 0.0																
MEDIUM 2																
NUCLEI NO.	Z NO.	A NO.	'GEOMETRIC' XSECT (PER CM)													
1	0.8000E 01	0.1600E 02	0.2852E-01													
TRANSPORT XSECTS FOR PARTICLE TYPES 1-7 IN MEDIUM 2 IN PER CM																
0.1088E 00 0.7168E-01 0.5242E-01 0.0 0.4356E-01 0.1158E-03 0.1158E-03																
MAX HYDROGEN XSECTS FOR PARTICLE TYPES 1-5 IN MEDIUM 2 IN PER CM																
0.8030E-01 0.4316E-01 0.1338E-01 0.0 0.4530E-02																
NCCL	NCAS	NAME	MAT	NMED	LELEM	NCART	NABCV	NELDO	NPART1	NPART2	NPART3	NPART4	NPART5	NPART6	BOLD	BLZ
1	1	1	1	1	0	0	0	0	0	0	0	0	0	0	00000042	00000042
	X	Y	Z		XC		YC	ZC		OLDWT	WT				E	EC
	0.6950E 00	0.0	0.6000E 02	0.0	0.6000E 02	0.0	0.0	0.0	0.0	0.1000E 01	0.1000E 01	0.7200E 03	0.0			
	U	V	U	V	TIP		APR	ZPR		EREC	EX	HEVSLM	UU			
	0.0	0.0	0.1000E 01	0.0	0.0		0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		
NCCL	NCAS	NAME	MAT	NMED	LELEM	NCART	NABCV	NELDO	NPART1	NPART2	NPART3	NPART4	NPART5	NPART6	BOLD	BLZ
2	1	1	1	1	1	2	1	14	2	2	16	2	2	00000042	00000042	
	X	Y	Z		XC		YC	ZC		OLDWT	WT				E	EC
	0.6950E 00	0.0	0.6000E 02	0.5531E 00	0.6000E 02	0.5531E 00	0.2897E-01	0.6320E 02	0.1000E 01	0.1000E 01	0.7200E 03	0.6841E 03	0.0			
	U	V	U	V	TIP		APR	ZPR		EREC	EX	HEVSLM	UU			
	-0.6978E-01	0.1130E-01	0.9975E 00	0.0	0.1101E 06	0.4505E 05	0.1614E 03	0.8371E 02	0.0	0.0	0.0	0.4759E 01				
NAMEA TIP A EA LA VA WA WTA																
2 0.1000E 01 0.5476E 03 -0.1595E 00 0.2626E 00 0.9516E 00 0.1000E 01																
TYPE FB LB VB *A WTH																
0.3000E 01 0.5539E 01 -0.6156E 00 0.3748E 00 0.6932E 00 0.1000E 01																
WTEVAP EFART ARRAY(EVAP NEUTRON ENERGY)																
0.1000E 01 0.4322E 01 0.1691E 01 0.0 0.4837E 01 0.5543E 01 0.8328E 00 0.4393E 01 0.0																
0.4436E 01 0.1810E 01 0.1667E 01 0.2529E 01 0.2728E 01 0.6987E 00																
ATEVAP EFART ARRAY(EVAP FROTON ENERGY)																
0.1000E 01 0.0 0.0																

Table III. (Cont'd)

ATEVAP - HEFART-ARRAY(EVAP-DEUTERON ENERGY)															
0.1000E 01 0.0 0.0															
ATEVAP HEFART ARRAY(EVAP TRITON ENERGY)															
0.1000E 01 0.0 0.0 0.8257E 02 0.3901E 02 0.0 0.1473E 01 0.7882E 02 0.5730L 02 0.0 0.3287E 01 0.0 0.1100E 03 0.1150E 03 0.4500E 02 0.4800E 02															
ATEVAP HEFART ARRAY(EVAP HE 3 ENERGY)															
0.1000E 01 0.0 0.0															
ATEVAP HEFART ARRAY(EVAP ALPHA ENERGY)															
0.1000E 01 0.0 0.0															
NCCL	NCCAS	NAME	NAT	NMEC	LELEM	NPART1	NABCV	NEELG	NPART2	NPART3	NPART4	NPART5	NPART6	BOLD	BLZ
														2	1
X														E	EC
0.5831E 00	0.2897E 01	0.6320E 02	0.2661E 00	0.5507E 00	0.659E 02	0.1000E 01	0.1000E 01	0.5476E 03	0.5476E 03						
V														UW	
-0.1595E 00	0.2626E 00	0.5516E 00	0.1000E 01	0.9112E 05	0.4005E 05	0.1458E 03	0.2903E 03	0.0	0.9741E 01						
NAMEA TIPA EA LA VA KA WTA															
3	0.3000E 01	0.4373E 02	-0.4540E 00	-0.3670E 00	-0.8062E 00	0.1000E 01									
4	0.0	0.3426E 02	0.1717E 00	0.8581E 00	0.4639E 00	0.1000E 01									
5	0.1000E 01	0.1927E 02	0.7731E 00	-0.1455E 00	-0.6173E 00	0.1000E 01									
6	0.1000E 01	0.1671E 02	-0.5875E 00	-0.5732E 00	-0.5712E 00	0.1000E 01									
7	0.1000E 01	0.2523E 02	0.8850E 00	0.2227E 00	0.4418E 00	0.1000E 01									
8	0.1000E 01	0.2194E 02	0.3762E 00	0.6643E 00	0.6400E 00	0.1000E 01									
9	0.1000E 01	0.1623E 02	-0.7757E 00	-0.2743E 00	-0.5684E 00	0.1000E 01									
10	0.0	0.9864E 01	-0.4039E 00	-0.3349E -02	0.9148E 00	0.1000E 01									
TIPB LB VB WB WTB															
0.1000E 01	0.9530E 01	0.6104E 00	-0.1950E 00	-0.7677E 00	0.1000E 01										
0.1000E 01	0.7847E 01	0.8039E 00	0.4200E 00	0.4212E 00	0.1000E 01										
0.1000E 01	0.2963E 01	-0.8672E 00	0.5977E -01	0.4933E 00	0.1000E V1										
ATEVAP HEFART ARRAY(EVAP NEUTRON ENERGY)															
0.1000E 01 0.0 0.0 0.4656E 01 0.0 0.1927E 02 0.1671E 02 0.2523E 02															
0.2194E 02 0.1623E 02 0.1095E 02 0.2002E 01 0.2599E 01 0.4548E 01 0.2787E 01 0.8591E 00															
0.0 0.3060E 01 0.2846E 01 0.1322E 01 0.5805E 01 0.2272E 01 0.3857E 00 0.3524E 01															
ATEVAP HEFART ARRAY(EVAP PROTON ENERGY)															
0.1000E 01 0.0 0.0															
ATEVAP HEFART ARRAY(EVAP DEUTERON ENERGY)															
0.1000E 01 0.0 0.0															
ATEVAP HEFART ARRAY(EVAP TRITON ENERGY)															
0.1000E 01 0.0 0.0 0.8621E 02 0.2201E 03 0.0 0.0 0.4631E 01 0.5963E 02															
0.7159E 02 0.0 0.5109E 01 0.0 0.9100E 02 0.1210E 03 0.4000E 02 0.5000E 02															
ATEVAP HEFART ARRAY(EVAP HE 3 ENERGY)															
0.1000E 01 0.0 0.0															
ATEVAP HEFART ARRAY(EVAP ALPHA ENERGY)															
0.1000E 01 0.0 0.0															
NCCL	NCCAS	NAME	NAT	NMEC	LELEM	NPART1	NABCV	NEELG	NPART2	NPART3	NPART4	NPART5	NPART6	BOLD	BLZ
														3	1
X														E	EC
0.2661E 00	0.5507E 00	0.6509E 02	0.2912E 00	0.6762E 00	0.6516E 02	0.1000E 01	0.1000E 01	0.3426E 02	0.1000E 01						
V														UW	
0.1717E 00	0.4581E 00	0.4839E 00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		
NCCL NCCAS NAME NAT NMEC LELEM NPART1 NABCV NEELG NPART2 NPART3 NPART4 NPART5 NPART6 BOLD BLZ															
6 1 5 1 1 1 0 0 0 8 2 2 16 2 2 00000042 00000042															
X														E	EC
0.2661E 00	0.5507E 00	0.6509E 02	0.2419E 01	0.1452E 00	0.6681E 02	0.1000E 01	0.1000E 01	0.1927E 02	0.1927E 02						

Table III. (Cont'd)

		TIP	APR	ZPR	EREC	EX	HEVSLM	UU								
0.7731E 00	-0.1456E 00	0.6173E 00	-0.1000E 03	-0.3151E 06	-0.4605E 05	0.1549E 03	-0.2621E 02	-0.0	-0.8926E 01							
*TEVAR		EFART ARRAY(EVAP NEUTRON ENERGY)														
0.1000E 01		0.5266E 01	0.0	0.3612E 01	0.2155E 01	0.1748E 01	0.0	0.3182E 01	0.2948E 01							
*TEVAR		EFART ARRAY(EVAP PROTON ENERGY)														
0.1000E 01		0.0	0.0													
*TEVAR		HEFART ARRAY(EVAP DEUTERON ENERGY)														
0.1000E 01		0.0	0.0													
*TEVAR		HEFART ARRAY(EVAP TRITON ENERGY)														
0.1000E 01		0.0	0.0	0.6197E 01	0.0	0.2894E 02	0.1150E 03	0.1180E 03	0.4600E 02							
*TEVAR		HEFART ARRAY(EVAP HE 3 ENERGY)														
0.1000E 01		0.0	0.0													
*TEVAR		HEFART ARRAY(EVAP ALPHA ENERGY)														
0.1000E 01		0.0	0.0													
NCCL	NCAS	NAME	MAT	NMED	LELEM	NOPART	NAPCV	NELD0	NPART1	NPART2	NPART3	NPART4	NPART5	NPART6	BOLD	BLZ
7	1	6	1	2	0	0	0	0	0	0	0	0	0	0	0.0000042	0.0001082
			X	Y	Z	XC	YC	ZC	CLDW	WT	E	F	EC			
			0.2661E 00	0.5507E 00	0.6509E 02	-0.3793E 01	-0.3410E 01	0.6115E 02	0.1000E 01	0.1000E 01	0.1671E 02	0.1671E 02				
			V	V	V	TIP	APR	ZPR	EREC	EX	HEVSLM	UU				
			-0.5875E 00	-0.5732E 00	-0.5712E 00	0.3000E 01	0.0	0.0	0.0	0.0	0.0	0.0				
NCCL	NCAS	NAME	MAT	NMED	LELEM	NOPART	NAPCV	NELD0	NPART1	NPART2	NPART3	NPART4	NPART5	NPART6	BOLD	BLZ
2	1	6	2	2	-1	2	1	1	0	0	0	0	0	0	0.0000082	0.0000081
			X	Y	Z	XC	YC	ZC	CLDW	WT	E	F	EC			
			-0.3793E 01	-0.3410E 01	0.6115E 02	-0.5520E 01	-0.5095E 01	0.5947E 02	0.1000E 01	0.1000E 01	0.1671E 02	0.1671E 02				
			V	V	V	TIP	APR	ZPR	EREC	EX	HEVSLM	UU				
			-0.5875E 00	-0.5732E 00	-0.5712E 00	0.3000E 01	0.0	0.0	0.0	0.0	0.0	0.0				
			NAMEA	TIPA	EA	LA	VA	WA	WTA							
			13	0.0	0.3979E 01	-0.6265E 00	0.4334E 00	-0.6478E 00	0.1000E 01							
			TIPF	EH	LB	VP	WE	WTB								
			0.1000E 01	0.1273E 02	-0.3244E 00	-0.8992E 00	-0.2938E 00	0.1000E 01								
NCCL	NCAS	NAME	MAT	NMED	LELEM	NOPART	NAPCV	NELD0	NPART1	NPART2	NPART3	NPART4	NPART5	NPART6	BOLD	BLZ
3	1	11	2	2	0	0	0	0	0	0	0	0	0	0	0.0000081	0.0000081
			X	Y	Z	XC	YC	ZC	CLDW	WT	E	F	EC			
			-0.5520E 01	-0.5095E 01	0.5947E 02	-0.5533E 01	-0.5086E 01	0.5945E 02	0.1000E 01	0.1000E 01	0.3979E 03	0.1000E 01				
			V	V	V	TIP	APR	ZPR	EREC	EX	HEVSLM	UU				
			-0.5855E 00	-0.4334E 00	-0.6478E 00	0.0	0.0	0.0	0.0	0.0	0.0	0.0				
NCCL	NCAS	NAME	MAT	NMED	LELEM	NOPART	NAPCV	NELD0	NPART1	NPART2	NPART3	NPART4	NPART5	NPART6	BOLD	BLZ
7	1	7	1	2	0	0	0	0	0	0	0	0	0	0	0.0000042	0.0001082
			X	Y	Z	XC	YC	ZC	CLDW	WT	E	F	EC			
			0.2661E 00	0.5507E 00	0.6509E 02	0.4804E 01	0.1714E 01	0.6740E 02	0.1000E 03	0.1000E 01	0.2523E 02	0.2523E 02				
			V	V	V	TIP	APR	ZPR	EREC	EX	HEVSLM	UU				
			0.8790E 00	0.2227E 00	0.4418E 00	0.1000E 01	C.0	0.0	0.0	0.0	0.0	0.0				
NCCL	NCAS	NAME	MAT	NMED	LELEM	NOPART	NAPCV	NELD0	NPART1	NPART2	NPART3	NPART4	NPART5	NPART6	BOLD	BLZ
2	1	7	2	2	-1	2	1	1	0	0	0	0	0	0	0.0000082	0.0000082
			X	Y	Z	XC	YC	ZC	CLDW	WT	E	F	EC			
			0.4760E 01	0.1714E 01	0.6740E 02	0.1027E 02	0.3166E 01	0.7018E 02	0.1000E 01	0.1000E 01	0.2523E 02	0.2523E 02				
			V	V	V	TIP	APR	ZPR	EREC	EX	HEVSLM	UU				
			0.5850E 00	0.2227E 00	0.4418E 00	0.1000E 01	C.0	0.0	0.0	0.0	0.0	0.0				
			NAMEA	TIPA	EA	LA	VA	WA	WTA							
			12	0.1000E 01	0.2496E 02	0.8988E 00	0.2630E 00	0.3506E 00	0.1000E 01							
			TIPP	EP	LB	VB	WE	WTB								

Table III. (Cont'd)

Table III. (Cont'd)

Table III. (Cont'd)

	X	Y	Z	XC	YC	ZC	OLDWT	WT	E	EC				
	U	0.3809E 01	0.3323E 01	0.8192E 02	0.2582E 02	0.3211E 02	0.1565E 03	0.1000E 01	0.1000E 01	0.1114E 03	0.1114E 03			
	U	0.2648E 00	0.3472E 00	0.8996E 00	0.1000E 01	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
NCCL	NOCAS	NAME	MAT	NNED	LELEM	KCPART	NABCV	NEELD	NPART1	NPART2	NPART3	NPART4	NPART5	NPART6
5	2	3	2	2	0	-1	0	0	0	0	0	0	0	0.0000043 0.0000043
	X	Y	Z	XC	YC	ZC	OLDWT	WT	E	EC				
	U	0.2582E 02	0.3211E 02	0.1565E 03	0.2855E 02	0.3080E 02	0.1688E 03	0.1000E 01	0.1000E 01	0.1114E 03	0.1114E 03			
	U	0.2648E 00	0.3472E 00	0.8996E 00	0.1000E 01	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
NCCL	NOCAS	NAME	MAT	NNED	LELEM	KCPART	NABCV	NEELD	NPART1	NPART2	NPART3	NPART4	NPART5	NPART6
5	2	3	2	2	0	-1	0	0	0	0	0	0	0	0.0000043 0.0000043
	X	Y	Z	XC	YC	ZC	OLDWT	WT	E	EC				
	U	0.2955E 02	0.3608E 02	0.1688E 03	0.2979E 02	0.3731E 02	0.1700E 03	0.1000E 01	0.1000E 01	0.1114E 03	0.1114E 03			
	U	0.2648E 00	0.3472E 00	0.8996E 00	0.1000E 01	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
NCCL	NOCAS	NAME	MAT	NNED	LELEM	KCPART	NABCV	NEELD	NPART1	NPART2	NPART3	NPART4	NPART5	NPART6
5	2	3	2	2	0	-1	0	0	0	0	0	0	0	0.0000043 0.0000043
	X	Y	Z	XC	YC	ZC	OLDWT	WT	E	EC				
	U	0.2979E 02	0.3731E 02	0.1700E 03	0.3001E 02	0.3761E 02	0.1708E 03	0.1000E 01	0.1000E 01	0.1114E 03	0.1114E 03			
	U	0.2648E 00	0.3472E 00	0.8996E 00	0.1000E 01	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
NCCL	NOCAS	NAME	MAT	NNED	LELEM	KCPART	NABCV	NEELD	NPART1	NPART2	NPART3	NPART4	NPART5	NPART6
5	2	3	2	2	0	-1	0	0	0	0	0	0	0	0.0000043 0.0000043
	X	Y	Z	XC	YC	ZC	OLDWT	WT	E	EC				
	U	0.3731E 02	0.1700E 03	0.3001E 02	0.3761E 02	0.1708E 03	0.1000E 01	0.1000E 01	0.1114E 03	0.1114E 03				
	U	0.2648E 00	0.3472E 00	0.8996E 00	0.1000E 01	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
NCCL	NOCAS	NAME	MAT	NNED	LELEM	KCPART	NABCV	NEELD	NPART1	NPART2	NPART3	NPART4	NPART5	NPART6
5	2	3	2	2	0	-1	0	0	0	0	0	0	0	0.0000043 0.0000043
	X	Y	Z	XC	YC	ZC	OLDWT	WT	E	EC				
	U	0.3761E 02	0.1708E 03	0.3179E 02	0.3938E 02	0.1768E 03	0.1000E 01	0.1000E 01	0.1114E 03	0.1114E 03				
	U	0.2648E 00	0.3472E 00	0.8996E 00	0.1000E 01	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
NCCL	NOCAS	NAME	MAT	NNED	LELEM	KCPART	NABCV	NEELD	NPART1	NPART2	NPART3	NPART4	NPART5	NPART6
2	2	3	2	2	0	-1	2	1	1	0	0	0	0	0.0000043 0.0000043
	X	Y	Z	XC	YC	ZC	OLDWT	WT	E	EC				
	U	0.3179E 02	0.1768E 03	0.3255E 02	0.4126E 02	0.1807E 03	0.1000E 01	0.1000E 01	0.1114E 03	0.1114E 03				
	U	0.2648E 00	0.3472E 00	0.8996E 00	0.1000E 01	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
	NAMEA	TIP	EA	LA	VAP	WA	WTA							
	6	0.0	0.1104E 03	0.2550E 00	0.4291E 00	0.8665E 00	0.1000E 01							
		TIP	EP	LR	VB	WB	WTB							
		0.1000E 01	0.9292E 00	0.1223E 00	-0.9010E 00	-0.4162E 00	0.1000E 01							
NCCL	NOCAS	NAME	MAT	NNED	LELEM	KCPART	NABCV	NEELD	NPART1	NPART2	NPART3	NPART4	NPART5	NPART6
4	2	3	2	2	0	-1	0	0	0	0	0	0	0	0.0000043 0.0000044
	X	Y	Z	XC	YC	ZC	OLDWT	WT	E	EC				
	U	0.3295E 02	0.4146E 02	0.1807E 03	0.3303E 02	0.4159E 02	0.1810E 03	0.1000E 01	0.1000E 01	0.1104E 03	0.1083E 03			
	U	0.2648E 00	0.4291E 00	0.8665E 00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
NCCL	NOCAS	NAME	MAT	NNED	LELEM	KCPART	NABCV	NEELD	NPART1	NPART2	NPART3	NPART4	NPART5	NPART6
6	2	3	2	4	1	1	0	0	10	2	16	2	2	0.0000042 0.0000042
	X	Y	Z	XC	YC	ZC	OLDWT	WT	E	EC				
	U	0.5737E 00	-0.1033E 01	0.7073E 02	-0.4850E 00	-0.8228E 00	0.7123E 02	0.1000E 01	0.1000E 01	0.5036E 02	0.5036E 02			
	U	0.8865E 00	0.1510E 00	0.4373E 00	0.1000E 01	0.1111E 06	0.4505E 05	0.1723E 03	0.5718E 02	0.0	0.1231E 02			
		WTEVAP	EFPART	ARRAY(EVAP_NELTRCN ENERGY)										
		0.1000E 01	0.1223E 01	0.2322E 01	0.1946E 01	0.0		0.2013E 01	0.2415E 01	0.4732E 01	0.0			
		WTEVAP	EFPART	ARRAY(EVAP_PRTCN ENERGY)										
		0.1000E 01	0.0	0.0										
		WTEVAP	EFPART	ARRAY(EVAP_DELTERCN ENERGY)										
		0.1000E 01	0.0	0.0										
		WTEVAP	EFPART	ARRAY(EVAP_TRTCN ENERGY)										
		0.1000E 01	0.0	0.0	0.0	0.0	0.0	0.2860E 02	0.0	0.7120E 01	0.8592E 02			
		WTEVAP	EFPART	ARRAY(EVAP_HE_3 ENERGY)										
		0.1000E 01	0.0	0.0										

Table III. (Cont'd)

WTEVAP HEARTY ARRAY(EVAP ALPHA ENERGY)																					
NCCL	NOCAS	NAME	MAT	NMED	LELEM	NPART	NPCV	NEELD	NPART1	NPART2	NPART3	NPART4	NPART5	NPART6	BOLD	BLZ					
5	2	5	1	1	0	-1	0	0	0	0	0	0	0	0.0000042	0.0000042						
	X	Y	Z	XC	YC	ZC	COLDWT	WT	E	EC											
	0.5707E	00	-0.1003E	01	0.7071E	02	0.1269E	03	-0.1157E	01	0.7284E	02	0.1000E	01	0.1000E	01	0.2023E	02	0.2023E	02	
	U	V	W	TIP	APR	ZPR	EREC	EX	HEVSLM	UU											
	0.3107E	00	-0.6849E	-01	0.9480E	00	0.1000E	01	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		
NCCL	NOCAS	NAME	MAT	NMED	LELEM	NPART	NPCV	NEELD	NPART1	NPART2	NPART3	NPART4	NPART5	NPART6	BOLD	BLZ					
5	2	5	1	1	0	-1	0	0	0	0	0	0	0	0.0000042	0.0000042						
	X	Y	Z	XC	YC	ZC	COLDWT	WT	E	EC											
	0.1269E	01	-0.1157E	01	0.7284E	02	0.3520E	01	-0.1653E	01	0.7971E	02	0.1000E	01	0.1000E	01	0.2023E	02	0.2023E	02	
	U	V	W	TIP	APR	ZPR	EREC	EX	HEVSLM	UU											
	0.3107E	00	-0.6849E	-01	0.9480E	00	0.1000E	01	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		
NCCL	NOCAS	NAME	MAT	NMED	LELEM	NPART	NPCV	NEELD	NPART1	NPART2	NPART3	NPART4	NPART5	NPART6	BOLD	BLZ					
7	2	5	1	2	0	-1	0	0	0	0	0	0	0	0.0000042	0.0001082						
	X	Y	Z	XC	YC	ZC	COLDWT	WT	E	EC											
	0.5520E	01	-0.1653E	01	0.7971E	02	0.4725E	01	-0.1919E	01	0.8339E	02	0.1000E	01	0.1000E	01	0.2023E	02	0.2023E	02	
	U	V	W	TIP	APR	ZPR	EREC	EX	HEVSLM	UU											
	0.3107E	00	-0.6849E	-01	0.9480E	00	0.1000E	01	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		
NCCL	NOCAS	NAME	MAT	NMED	LELEM	NPART	NPCV	NEELD	NPART1	NPART2	NPART3	NPART4	NPART5	NPART6	BOLD	BLZ					
5	2	5	2	2	0	-1	0	0	0	0	0	0	0	0.0001082	0.0000082						
	X	Y	Z	XC	YC	ZC	COLDWT	WT	E	EC											
	0.4725E	01	-0.1919E	01	0.8339E	02	0.6248E	01	-0.2254E	01	0.8804E	02	0.1000E	01	0.1000E	01	0.2023E	02	0.2023E	02	
	U	V	W	TIP	APR	ZPR	EREC	EX	HEVSLM	UU											
	0.3107E	00	-0.6849E	-01	0.9480E	00	0.1000E	01	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		
NCCL	NOCAS	NAME	MAT	NMED	LELEM	NPART	NPCV	NEELD	NPART1	NPART2	NPART3	NPART4	NPART5	NPART6	BOLD	BLZ					
5	2	5	2	2	1	-1	0	0	0	0	0	0	0	0.0000082	0.0000082						
	X	Y	Z	XC	YC	ZC	COLDWT	WT	E	EC											
	0.6248E	01	-0.2254E	01	0.8804E	02	0.9167E	01	-0.2898E	01	0.9594E	02	0.1000E	01	0.1000E	01	0.2023E	02	0.2023E	02	
	U	V	W	TIP	APR	ZPR	EREC	EX	HEVSLM	UU											
	0.3107E	00	-0.6849E	-01	0.9480E	00	0.1000E	01	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		
NCCL	NOCAS	NAME	MAT	NMED	LELEM	NPART	NPCV	NEELD	NPART1	NPART2	NPART3	NPART4	NPART5	NPART6	BOLD	BLZ					
2	2	5	2	2	1	-1	2	1	0	0	0	0	0	0.0000082	0.0000082						
	X	Y	Z	XC	YC	ZC	COLDWT	WT	E	EC											
	0.9167E	01	-0.2898E	01	0.9594E	02	0.1044E	02	-0.3179E	01	0.1000E	03	0.1000E	01	0.1000E	01	0.2023E	02	0.2023E	02	
	U	V	W	TIP	APR	ZPR	EREC	EX	HEVSLM	UU											
	0.3107E	00	-0.6849E	-01	0.9480E	00	0.1000E	01	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		
	NAME	TIPA	EA	LA	VA	WA	WTA														
7	U	0	0.1144E	02	-0.3791E	00	0.5913E	-01	0.9235E	00	0.1000E	01									
	TIPA	EB	LB	VR	WB	WTB															
	0.1000E	01	0.8793E	01	0.9054E	00	-0.1717E	00	0.3884E	00	0.1000E	01									
NCCL	NOCAS	NAME	MAT	NMED	LELEM	NPART	NPCV	NEELD	NPART1	NPART2	NPART3	NPART4	NPART5	NPART6	BOLD	BLZ					
3	2	7	2	2	0	0	0	0	0	0	0	0	0	0	0.0000082	0.0000082					
	X	Y	Z	XC	YC	ZC	COLDWT	WT	E	EC											
	0.1044E	02	-0.3179E	01	0.1000E	03	0.1039E	02	-0.3179E	01	0.1010E	03	0.1000E	01	0.1000E	01	0.1144E	02	0.1000E	01	
	U	V	W	TIP	APR	ZPR	EREC	EX	HEVSLM	UU											
	-0.3791E	00	0.5913E	-01	0.9235E	00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		

With the above information, looking at Table III for particle event 2 of the first history, one knows there was a fission and that only neutrons were evaporated. In particular, two prefission evaporation neutrons were produced, four postfission evaporation neutrons were produced from the first fission fragment, and six postfission evaporation neutrons were produced from the second fission fragment. The last 13 values in the triton table (after third zero value) give the fragment data as follows:

I = 3 (for this particle event since no tritons
were evaporated).

HEPART(I+1,2) = ERN1, the kinetic recoil energy of the first
fragment after evaporation. (ERN1 = 82.57)

HEPART(I+2,2) = El, the excitation energy of the first fragment
prior to evaporation. (El = 39.01)

HEPART(I+3,2) = HEVS1, sum of the kinetic energies of all
charged particles, except protons, emitted during
evaporation from the first fragment. (HEVS1 = 0.0)

HEPART(I+4,2) = USE1, the excitation energy of the first fragment
residual after evaporation. (USE1 = 1.473)

HEPART(I+5,2) = ERN2, the kinetic recoil energy of the second
fragment after evaporation. (ERN2 = 78.82)

HEPART(I+6,2) = E2, the excitation energy of the second fragment
prior to evaporation. (E2 = 57.30)

HEPART(I+7,2) = HEVS2, sum of the kinetic energies of all
charged particles, except protons, emitted during
evaporation from the second fragment. (HEVS2 = 0.0)

HEPART(I+8,2) = USE2, the excitation energy of the second frag-
ment residual after evaporation. (USE2 = 3.287)

HEPART(I+9,2) = HEVSO, sum of the kinetic energies of all charged particles, except protons, emitted during evaporation from the original nucleus.
 (HEVSO = 0.0)

HEPART(I+10,2) = APR1, mass number A, of the first fission fragment.
 (APR1 = 110.0)

HEPART(I+11,2) = APR2, mass number, A, of the second fission fragment. (APR2 = 115.0)

HEPART(I+12,2) = ZPR1, charge number, Z, of the first fission fragment. (ZPR1 = 45.0)

HEPART(I+13,2) = ZPR2, charge number, Z, of the second fission fragment. (ZPR2 = 48.0)

The header information for this particle event contains some fragment data combined as follows:

APR = 1000*APR1+APR2 (APR = 0.1101E06)

ZPR = 1000*ZPR1+ZPR2 (ZPR = 0.4505E05)

EREC = ERN1+ERN2, the sum of the kinetic recoil energies of both fission fragments after evaporation. (EREC = 0.1614E03)

HEVSUM = HEVSO+HEVS1+HEVS2, sum of the kinetic energies of all charged particles, except protons, emitted during evaporation. (HEVSUM = 0.0)

UU = USE1+USE2, the sum of the excitation energies of both fission fragments after evaporation.
 (UU = 0.4759E01)

The next particle event also describes a nuclear interaction in which fission occurred.

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